

# CC-218 VOL BOARD

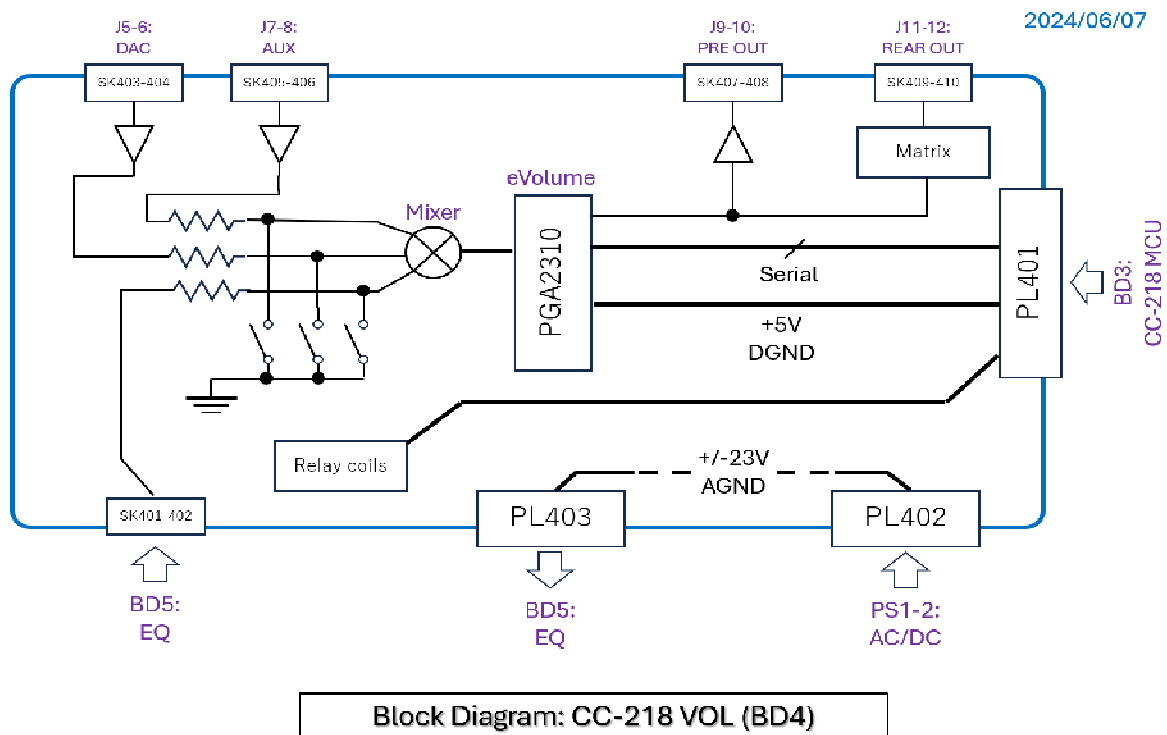
## Design

2023/08/20

2025/06/08

## *Circuit Design*

### Block Diagram



## Contents:

## Simulation of Selector

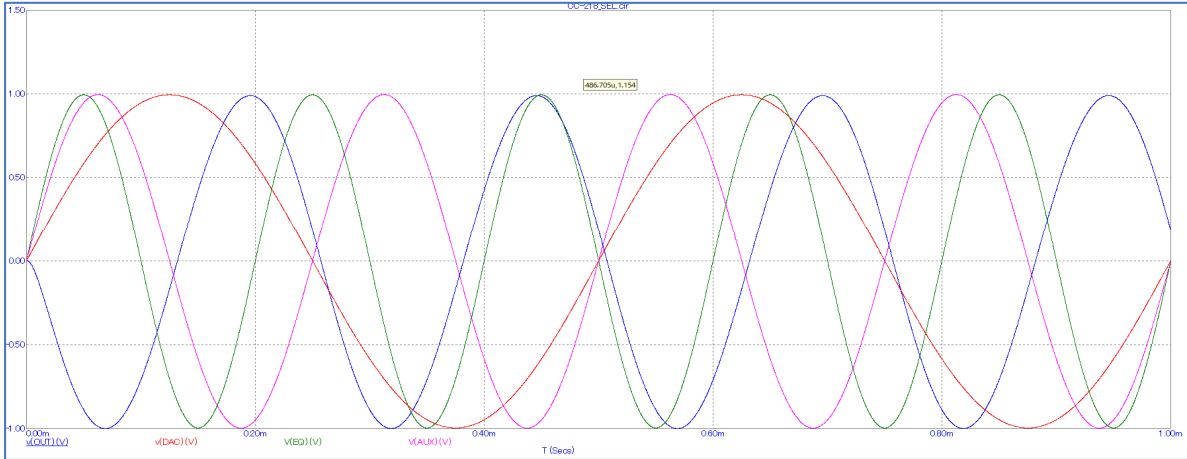
## Simulation of Matrix

## Schematic

## Power Dissipation

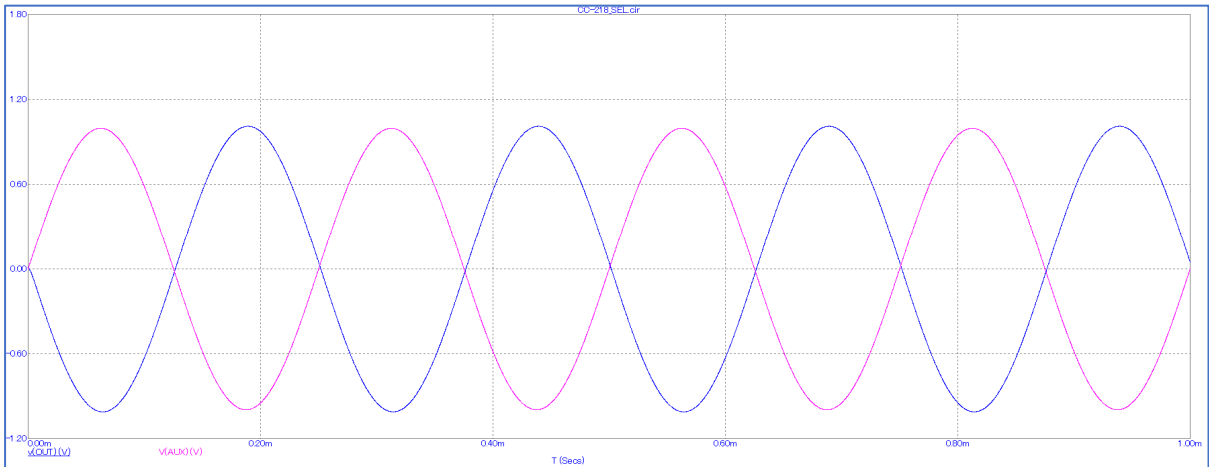


EQ, DAC, AUX ==> OUT



EQ: 5kHz, 1Vpeak  
DAC: 2kHz, 1Vpeak  
AUX: 4kHz, 1Vpeak

AUX ==> OUT



The waveform seems right.

\* AC analysis

Settings

AC Analysis Limits

Run Add Delete Expand... Stepping... Properties... Help...

Frequency Range: Log 1000k, 1  
Number of Points: 1001  
Temperature: Linear 27  
Maximum Change %: 5  
Noise Input: NONE  
Noise Output: 2

Run Options: Normal  
State Variables: Zero

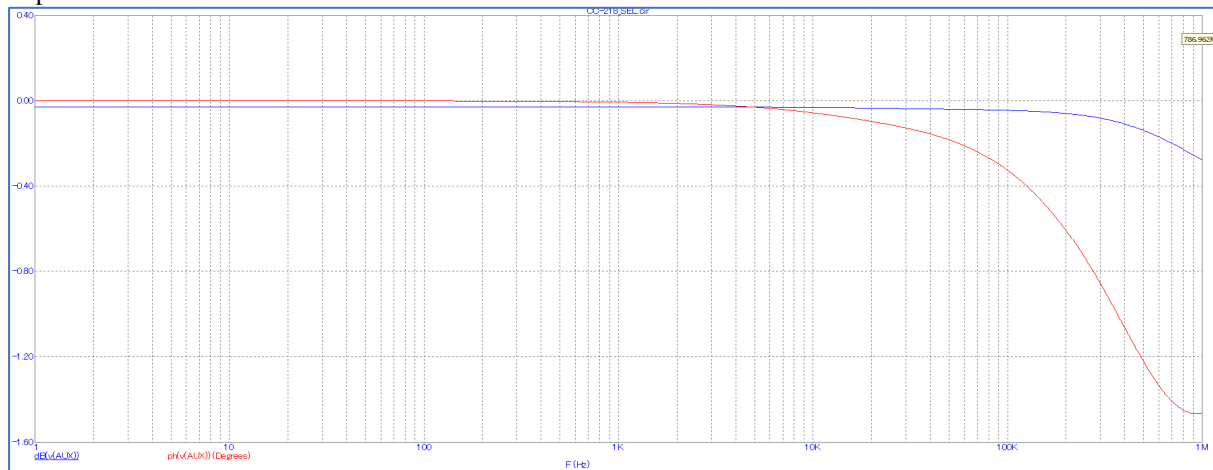
☒ Operating Point  
☒ Auto Scale Ranges  
☐ Accumulate Plots

☐ Ignore Expression Errors

Page	P	X Expression	Y Expression	X Range	Y Range	>
1	F		dB(v(AUX))	1e+6, 1, 200000	0.4, -1.6, 0.4	
1	F		ph(v(AUX))	1e+6, 1, 200000	0.4, -1.6, 0.4	
2	F		db(v(OUT))	1e+6, 1, 200000	10, -15, 5	
2	F		ph(v(OUT))	1e+6, 1, 200000	240, -60, 60	

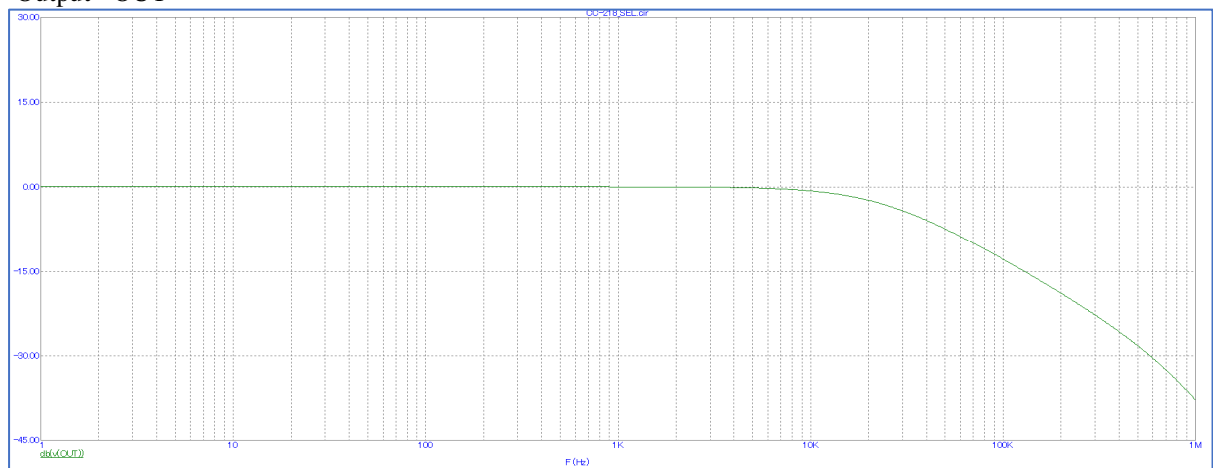
Runs the analysis.

Input - AUX



Freq resp is flat till 100kHz.

Output - OUT

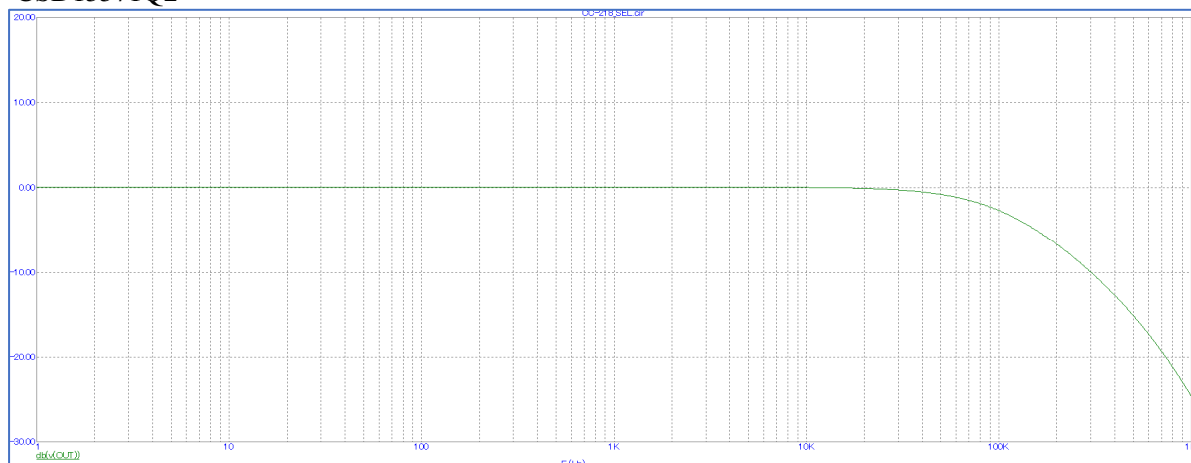


Treble rolls off!!!

It's probably due to the capacitance of IRFP460.

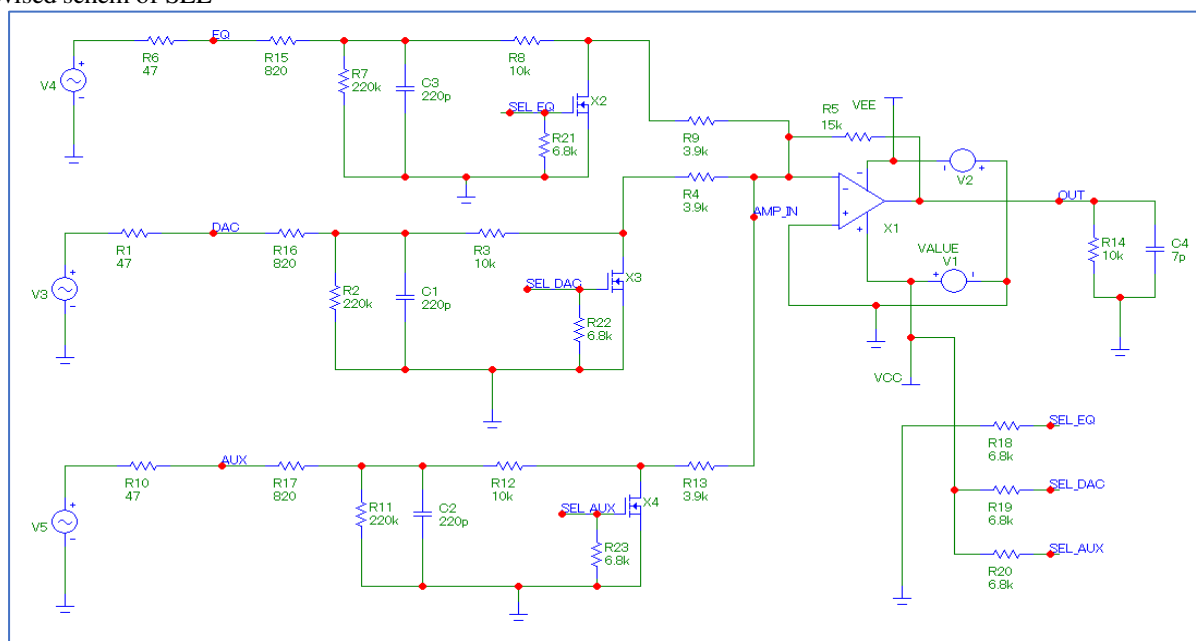
==> Replace IRFP460 w/ CSD15571Q2

## CSD15571Q2



Treble still rolls off but the cutoff frequency is higher.  
 GSF2301 may raise the cutoff frequency, because it has smaller capacitance.  
 Unfortunately, the SPICE model of GSF2301 is not available.

## \* Revised schem of SEL



Op amp: OPA627

N-MOSFET: CSD15571Q2

In the figure above, EQ is selected.

\* THD

Settings

Harmonic Distortion Analysis Limits

Run

Add

Delete

Expand...

Stepping...

PSS...

Properties...

Help...

Fundamental Frequency

List

1K

Name of Input Source

V4

Input Source Amplitude

Log

100m, 1m, 2

Name of Source Resistor

None

Name of Load Resistor

R14

Noise Frequency Range

100K, 1

Temperature

Linear

27

Max Simulation Cycles

50

Steady State Tolerance

1u

Time Step Ratio

1m

Highest Harmonic in THD

7

Number of Time Points

51

Number of Frequency Points

51

Run Options

Normal

State Variables

Zero

☒ Operating Point

☒ Auto Scale Ranges

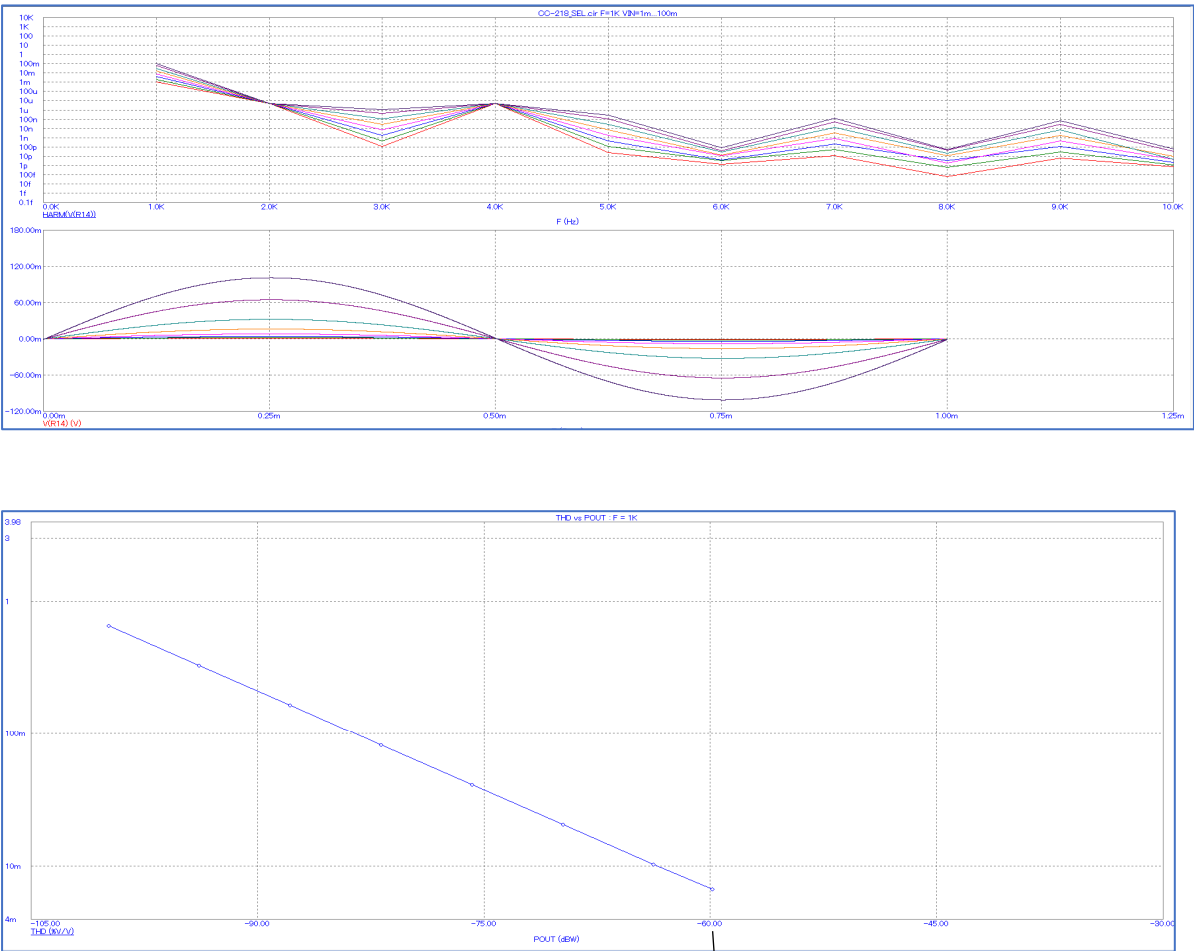
☐ Accumulate Plots

☒ Periodic Steady State

☐ Ignore Expression Errors

	Page	P	X Expression	Y Expression	X Range	Y Range
<input checked="" type="checkbox"/>		1	F	HARM(V(R14))	10000,0,1000	10000,1e-16
<input checked="" type="checkbox"/>		2	T	V(R14)	0.00125,0,0.000	0.18,-0.12,0.06
<input checked="" type="checkbox"/>			F	THD(HARM(V(R14)))	10000,0,1000	1,0,0.2
<input checked="" type="checkbox"/>			F	THDN(HARM(V(R14)))	10000,0,1000	5,0,1
<input checked="" type="checkbox"/>			F	HARM(I(V4))	10000,0,1000	1,1e-20
<input checked="" type="checkbox"/>					Auto	Auto

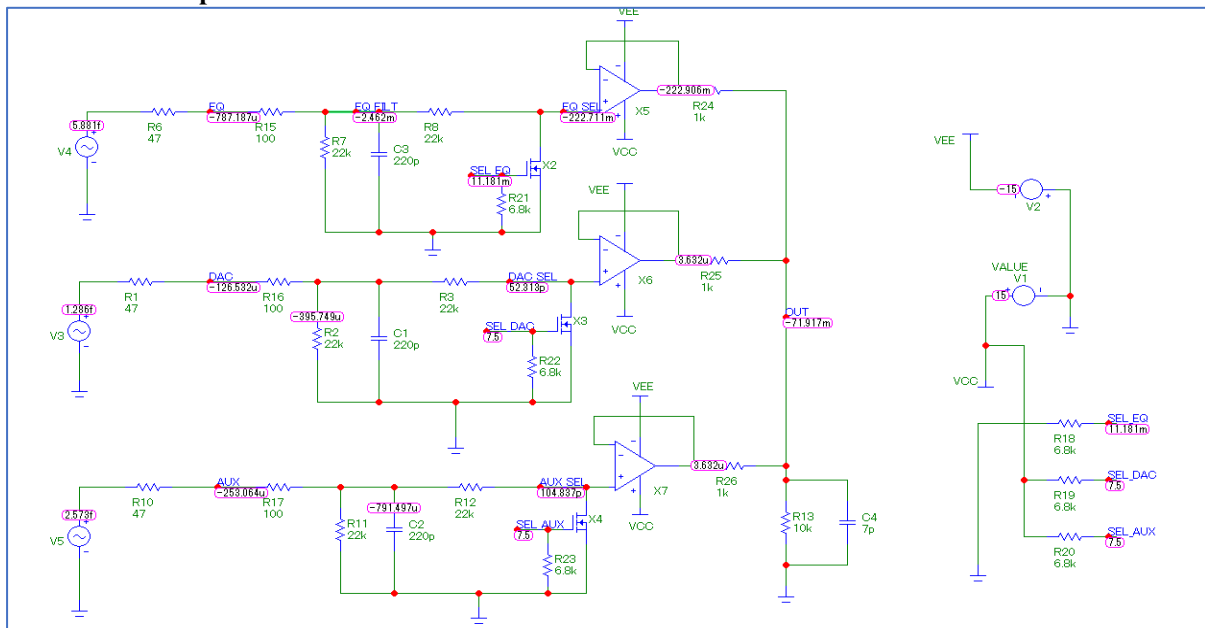
Result



Too large harmonics!

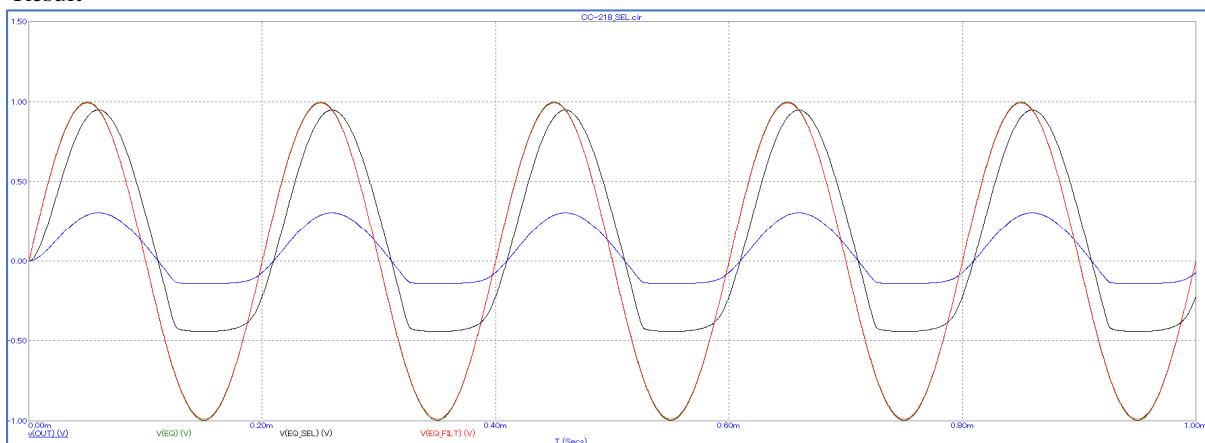
1uW (100mV into 10kohm)

**\* Alternative circuit - passive adder**



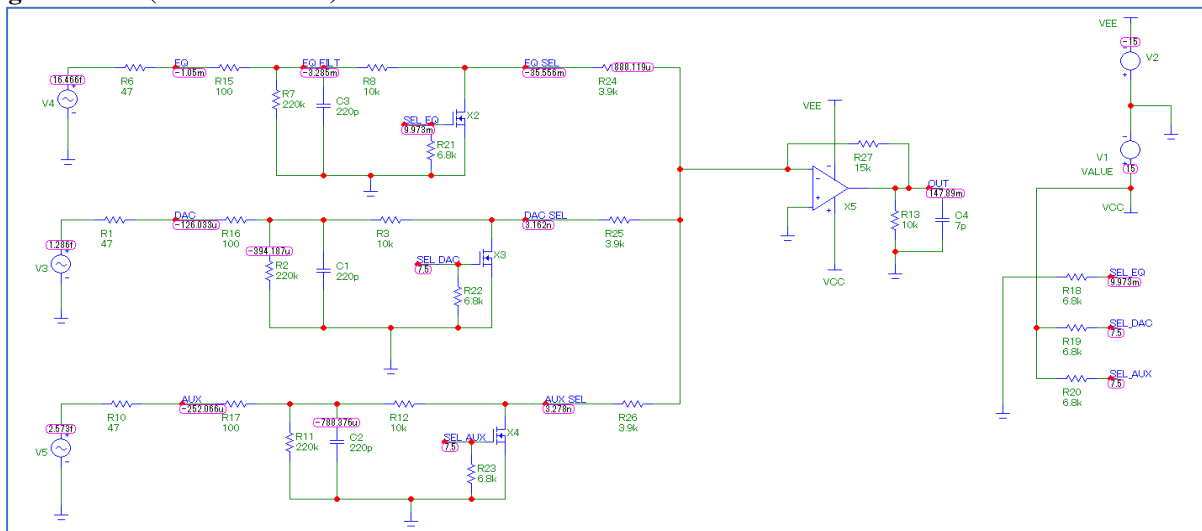
Passive adder

**Result**

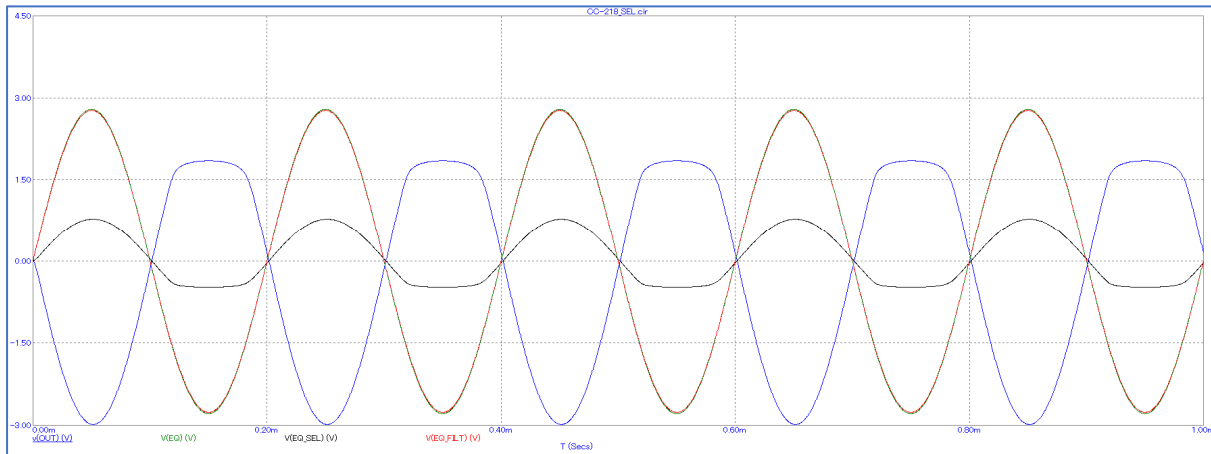


NMOS acts as diode clamp!  
EQ\_SEL can't swing below 0.44V

## \* Original circuit (redrawn schem)

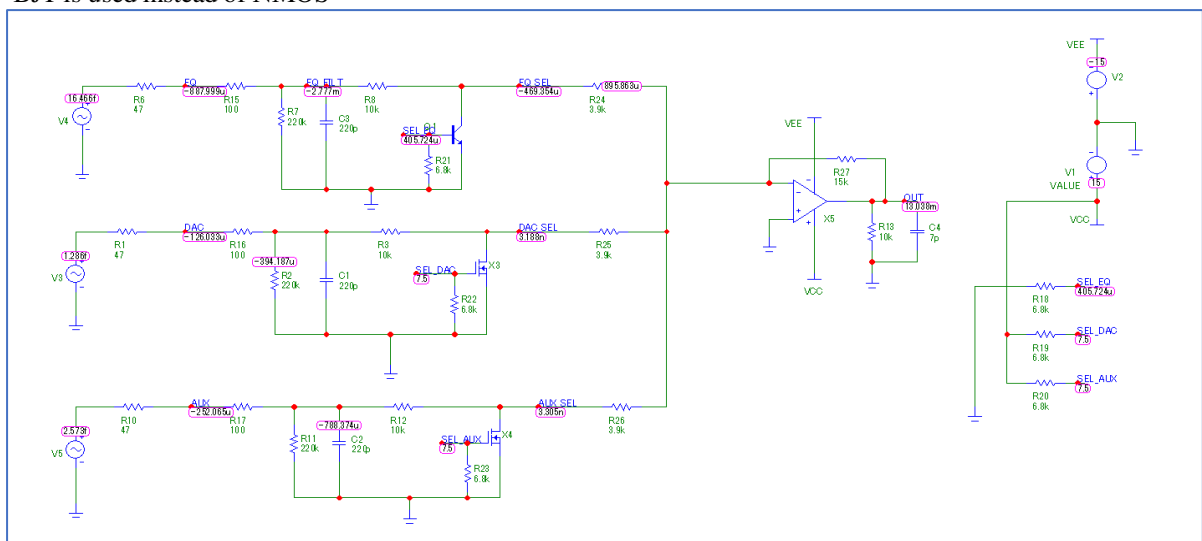


## Result



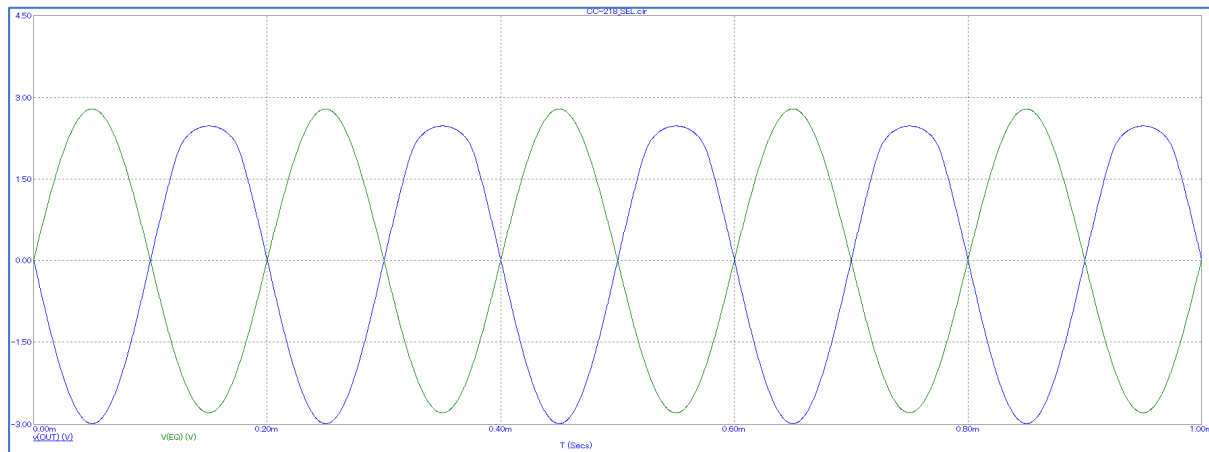
The level of EQ (V4) is increased  $2.8V_{\text{peak}} (=2V_{\text{rms}})$   
 $\Rightarrow$  EQ\_SEL is clumped!

## BJT is used instead of NMOS



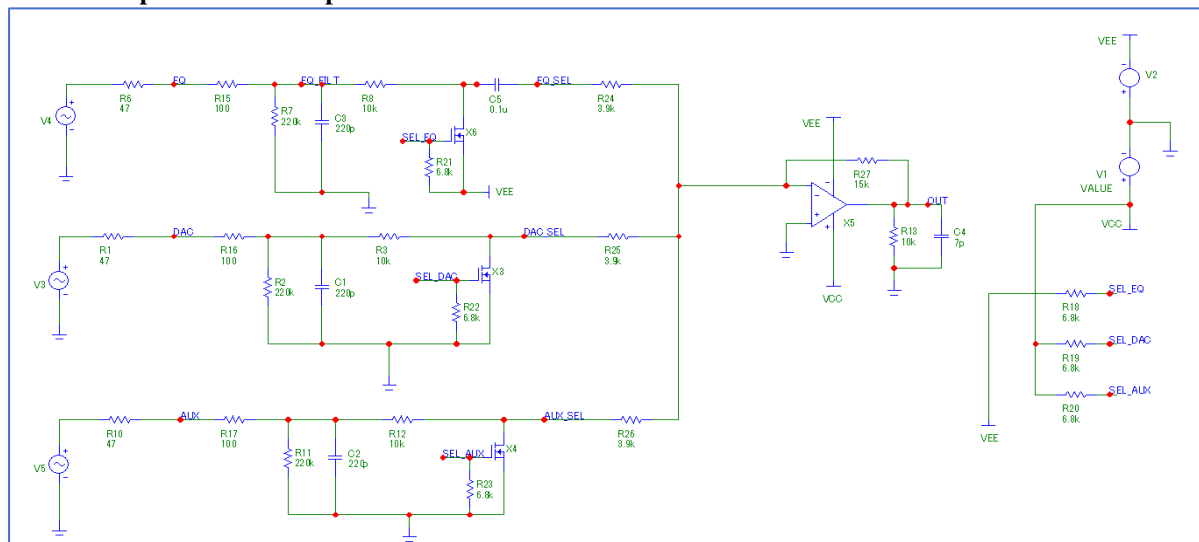


## Result



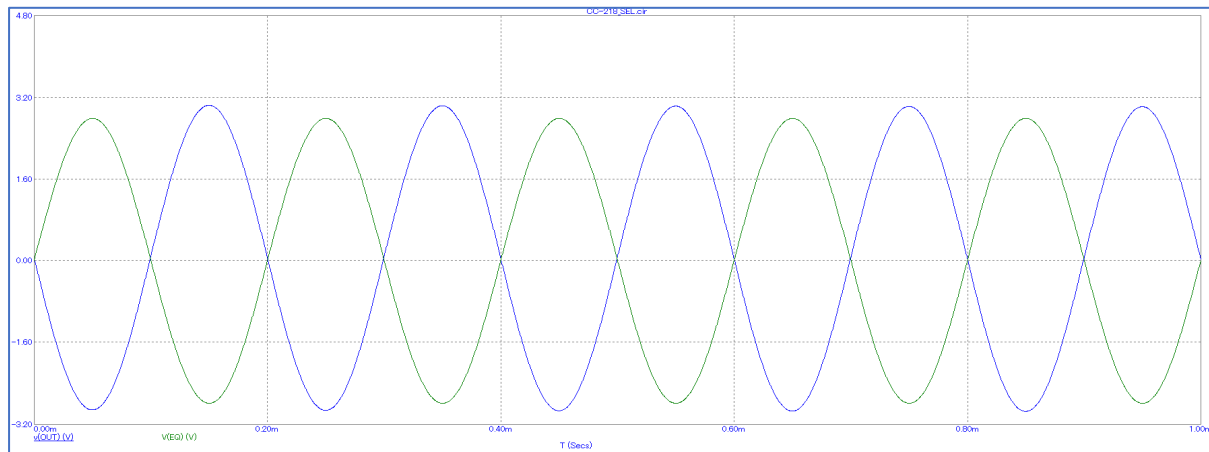
Output still distorted!

\* Another attempt - NMOS clumped to VEE



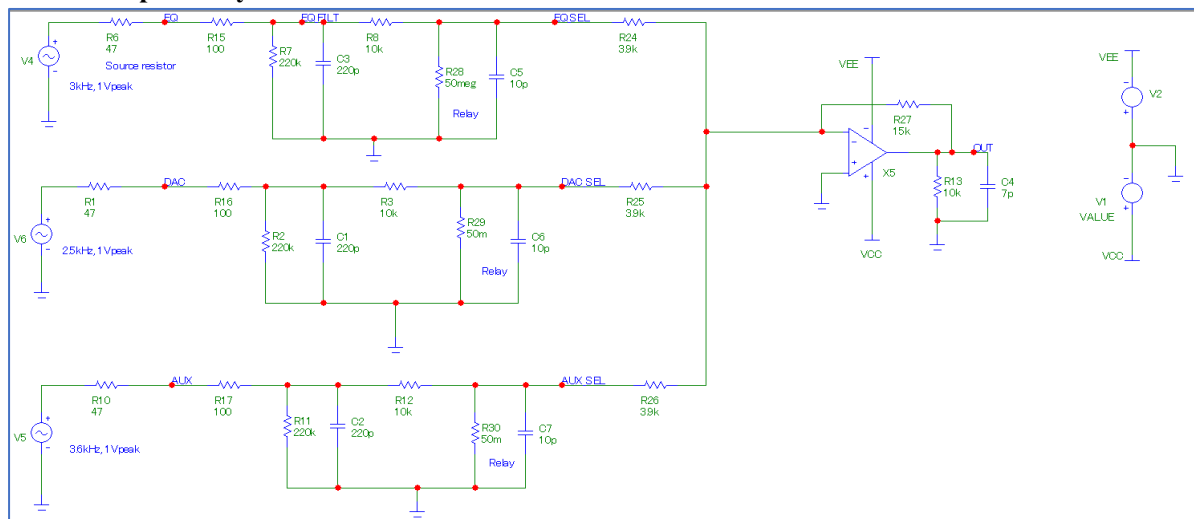
The source of NMOS connected to VEE (-15V)  
AC coupling to the adder

## Result

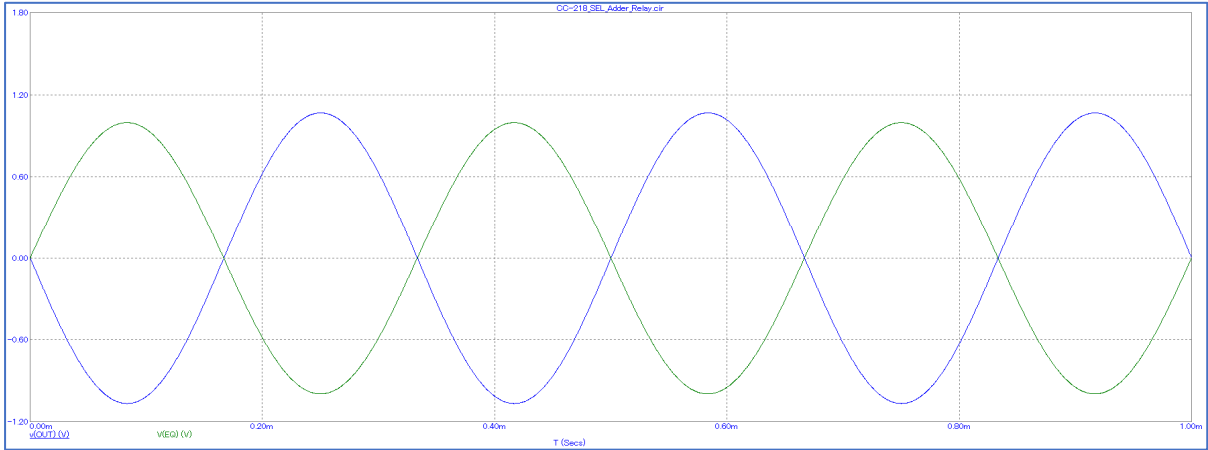


Less distortion!

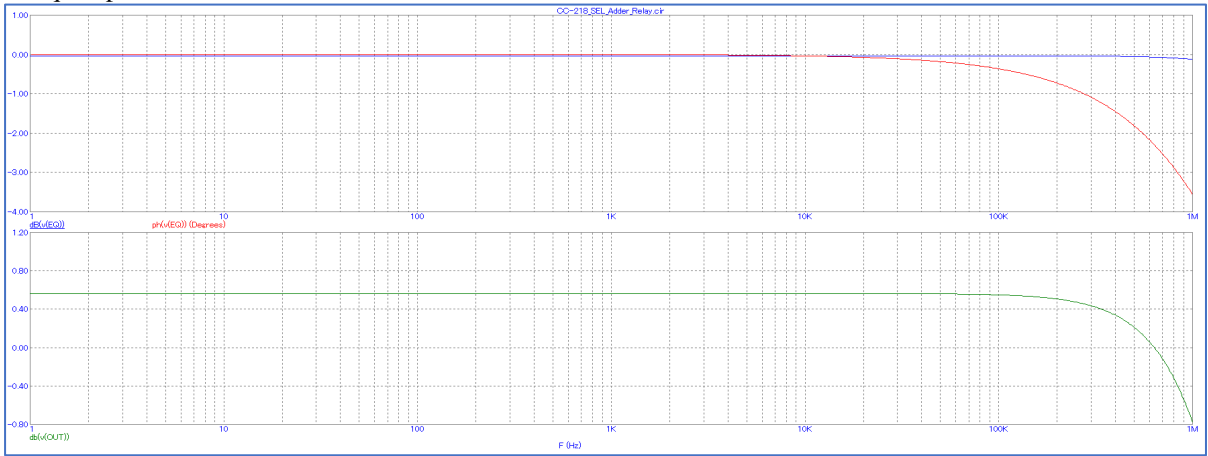
\* Another attempt - Relays used for shunt



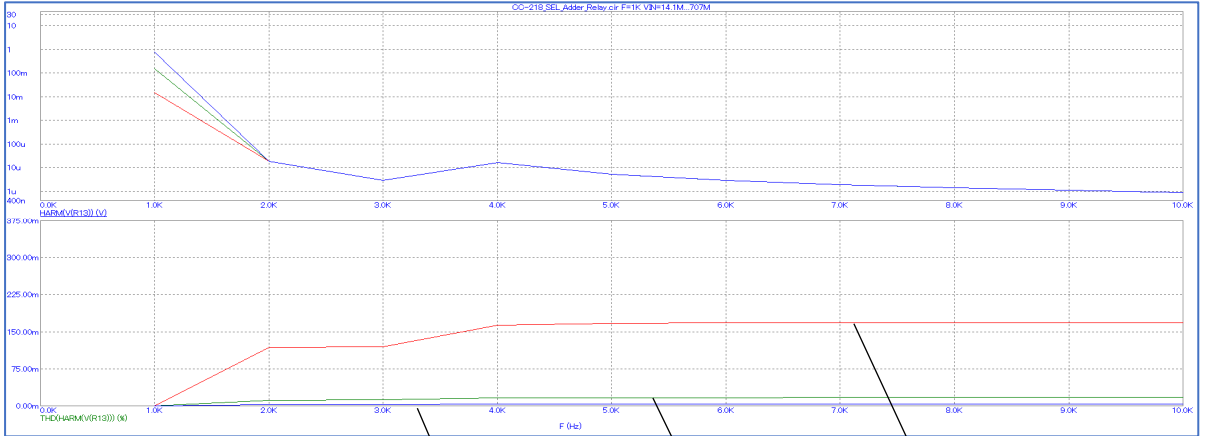
Transient response - sine wave



Freq Resp



Harmonic distortion

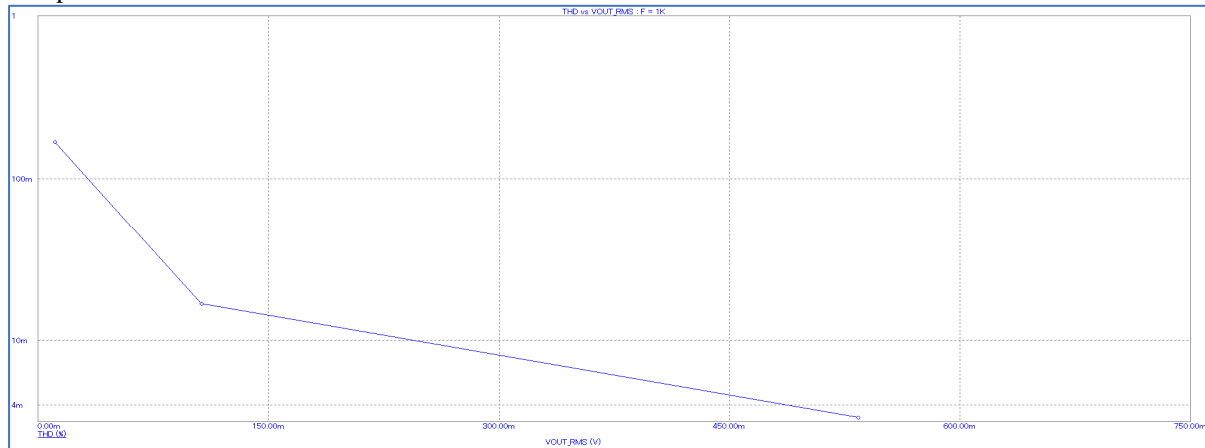


0.004% for  
Vin=0.5Vrms

0.017% for  
Vin=100mVrms

0.17% for  
Vin=10mVrms

Output vs THD



Tips on MC-12: Click the chart above, then the following dialog appears.

Properties for Harmonic Distortion Plot: THD vs VOUT\_RMS : F = 1K

Plot | Scales and Formats | Colors, Fonts, and Lines | Scope | Header | Numeric Output | Tool Bar

Curves: ☒ THD vs. VOUT\_RMS

Add Delete

Plot Group: 1

Labels: ☒ Show Font... ☒ Update During Run

Title: THD vs VOUT\_RMS : F = 1K ☒ Auto

X Axis: ☐ F ☐ VIN ☒ VOUT ☐ PIN ☐ POUT

Show As: ☐ dB ☐ dBm ☒ Number

All

Y Axis: ☒ THD ☐ THDN ☐ SINAD ☐ SNR ☐ H ☐ Gain ☐ Phase

Type: ☒ Voltage ☐ Power

Show As: ☒ % ☐ dB ☐ dBm ☐ Number

All

Form: ☐ Peak ☒ RMS

Designator: ☒ Simple ☐ Literal All

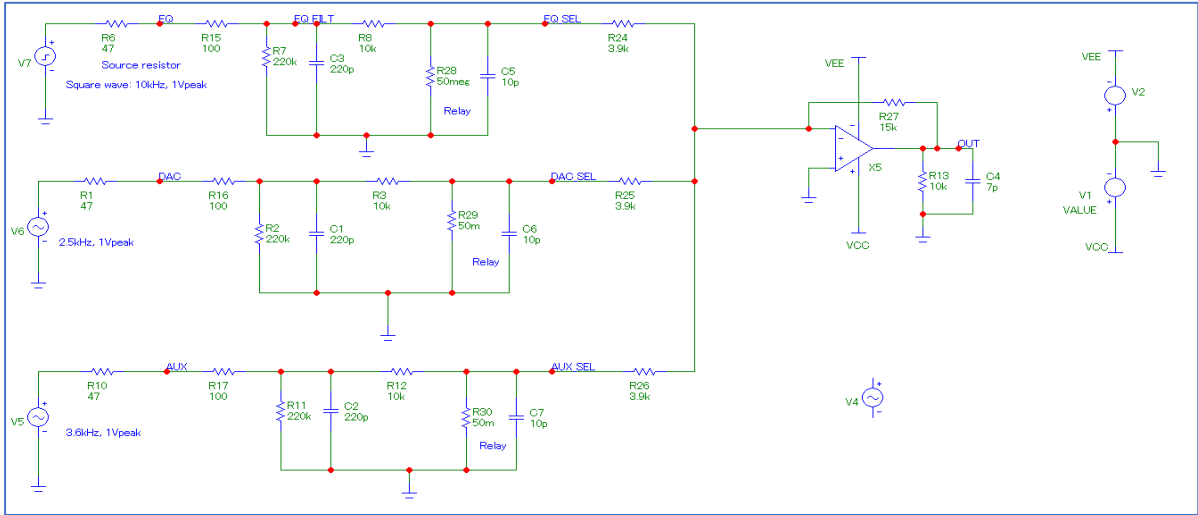
Buffer:

What Run to Plot: VIN: 14.1M

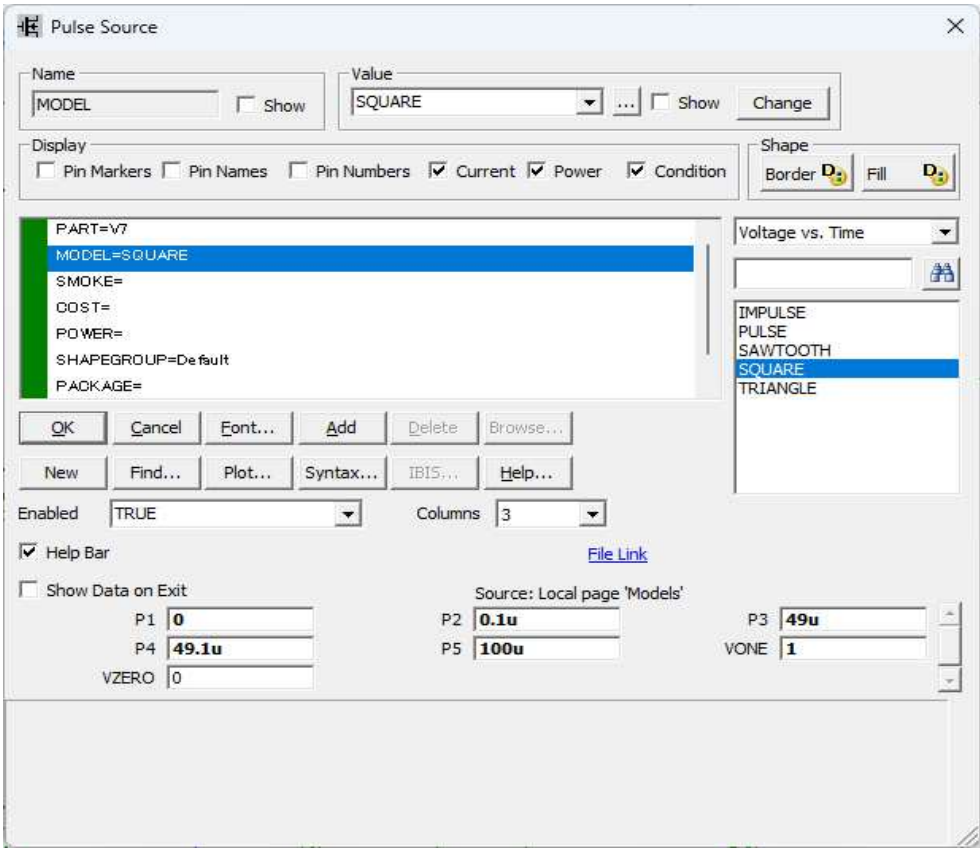
OK キャンセル 適用(A) ヘルプ

Select the options indicated by the red circles.

Square wave response

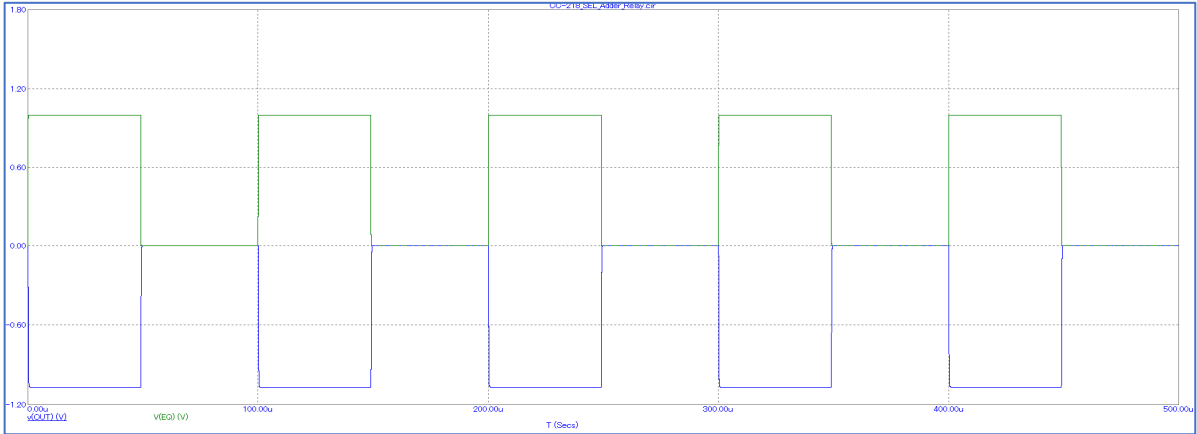


Settings of square wave source



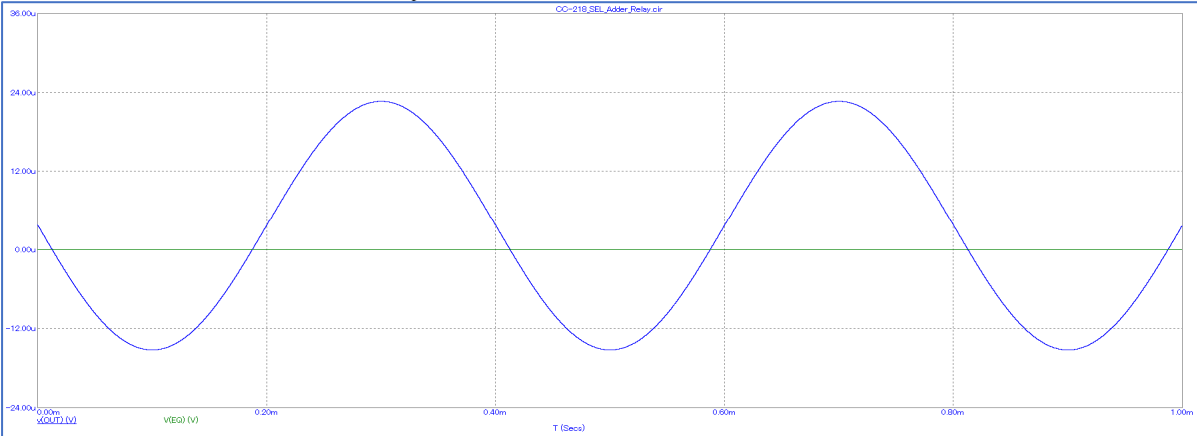
10kHz square wave

Result



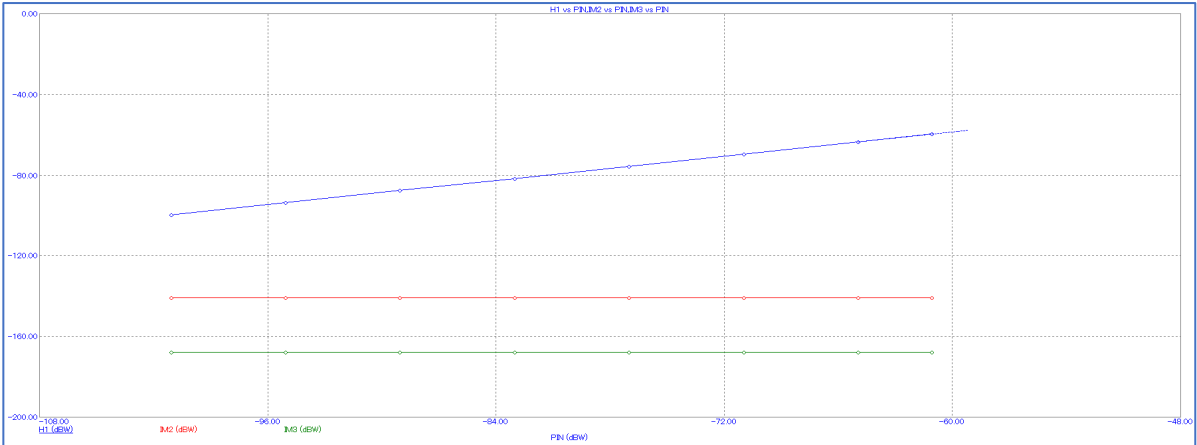
Crosstalk

EQ selected, EQ=0V, DAC=1V<sub>peak</sub>, AUX=0V



Crosstalk from DAC: 19uV<sub>peak</sub>... -94.4dB

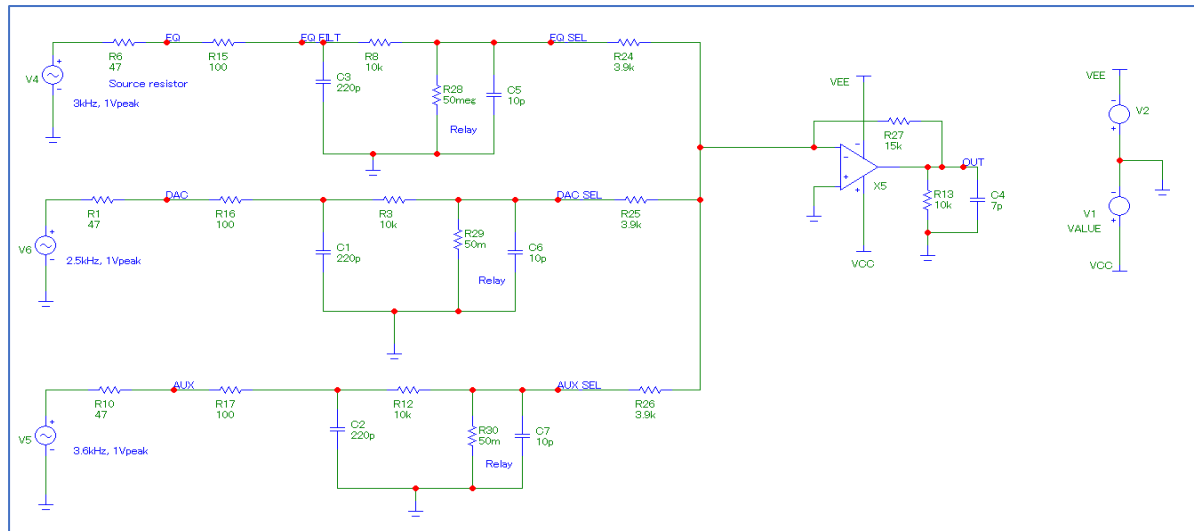
IMD



### \* Conclusion

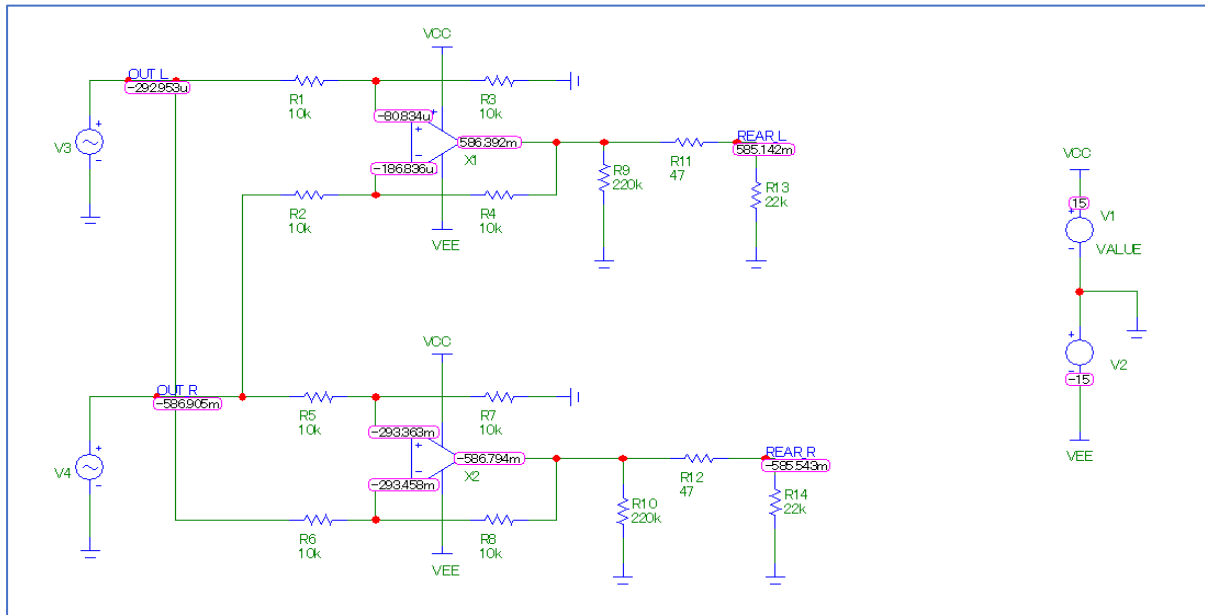
Relay + Adder is the best solution!

### Final circuit



## Simulation of Matrix

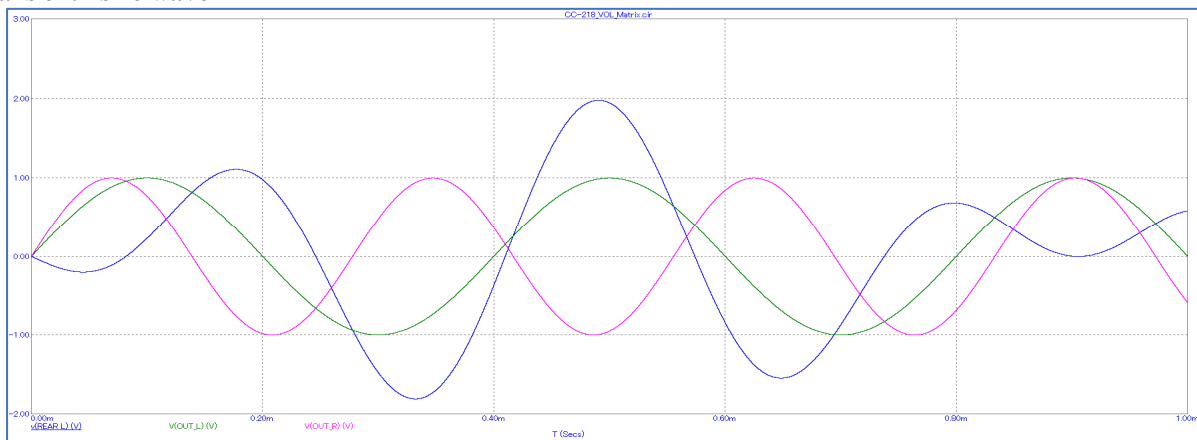
### \* Schematics for simulation



Op amp: LME49860 (similar to LME49720)

Original schem is wrong: R3 and R7 are connected to the output!

### \* Transient - sine wave

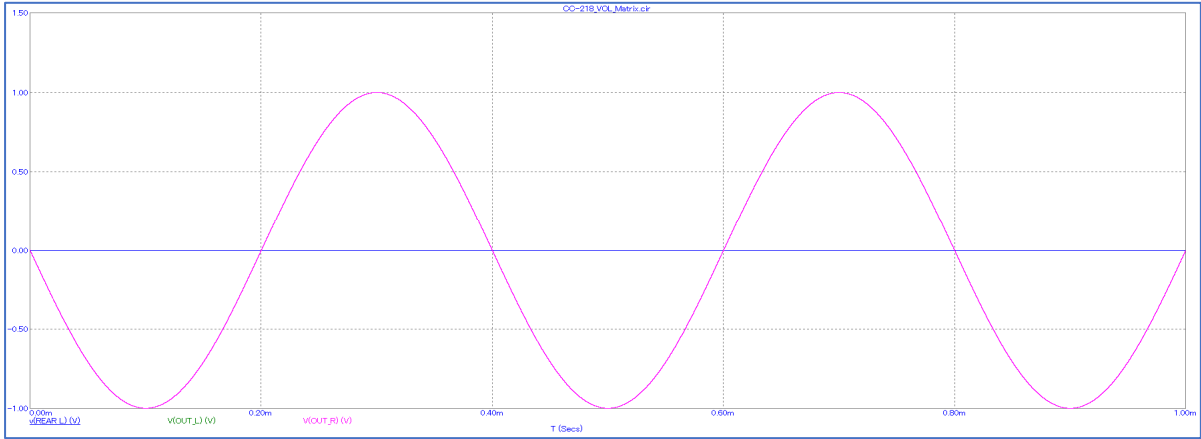


V3 (OUT\_L): 2.5kHz, 1V<sub>peak</sub>

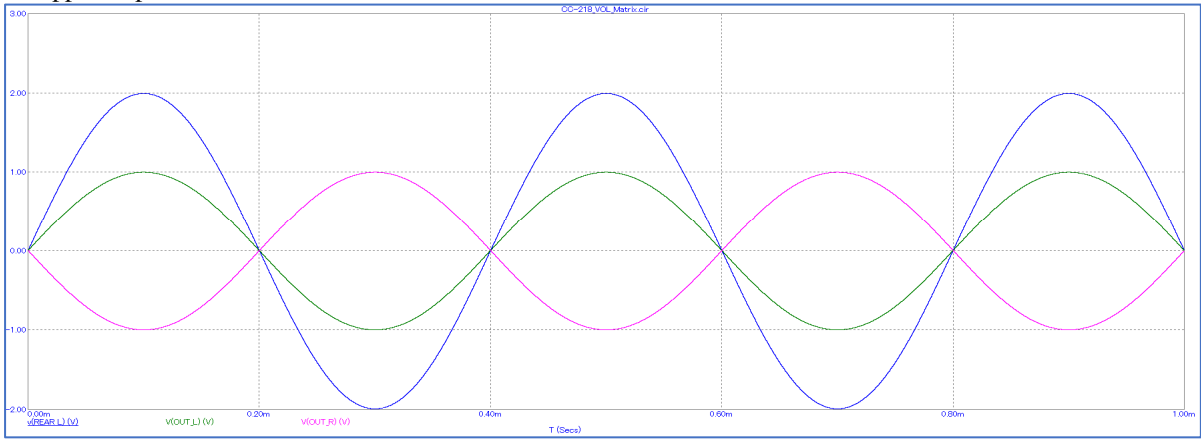
V4 (OUT\_R): 3.6kHz, 1V<sub>peak</sub>



In phase

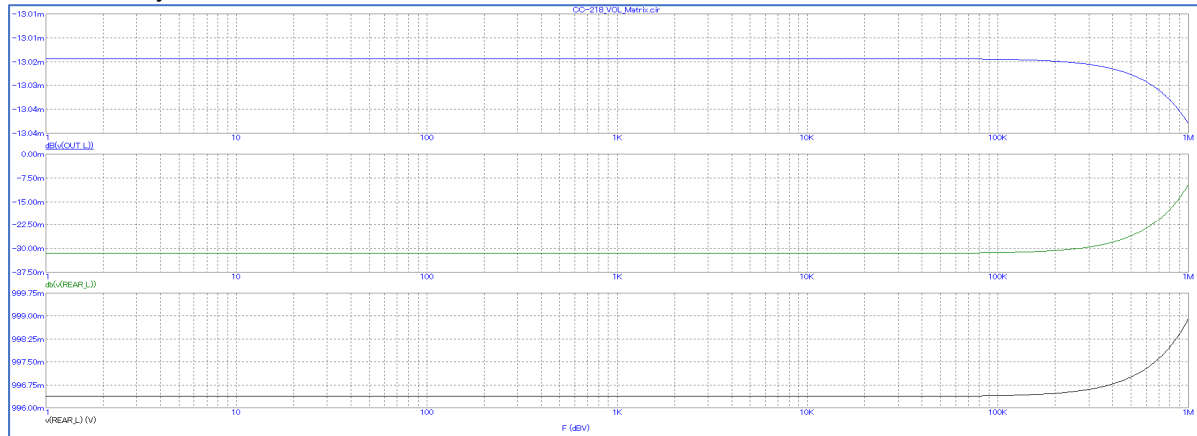


In opposite phase



**\* Freq resp**

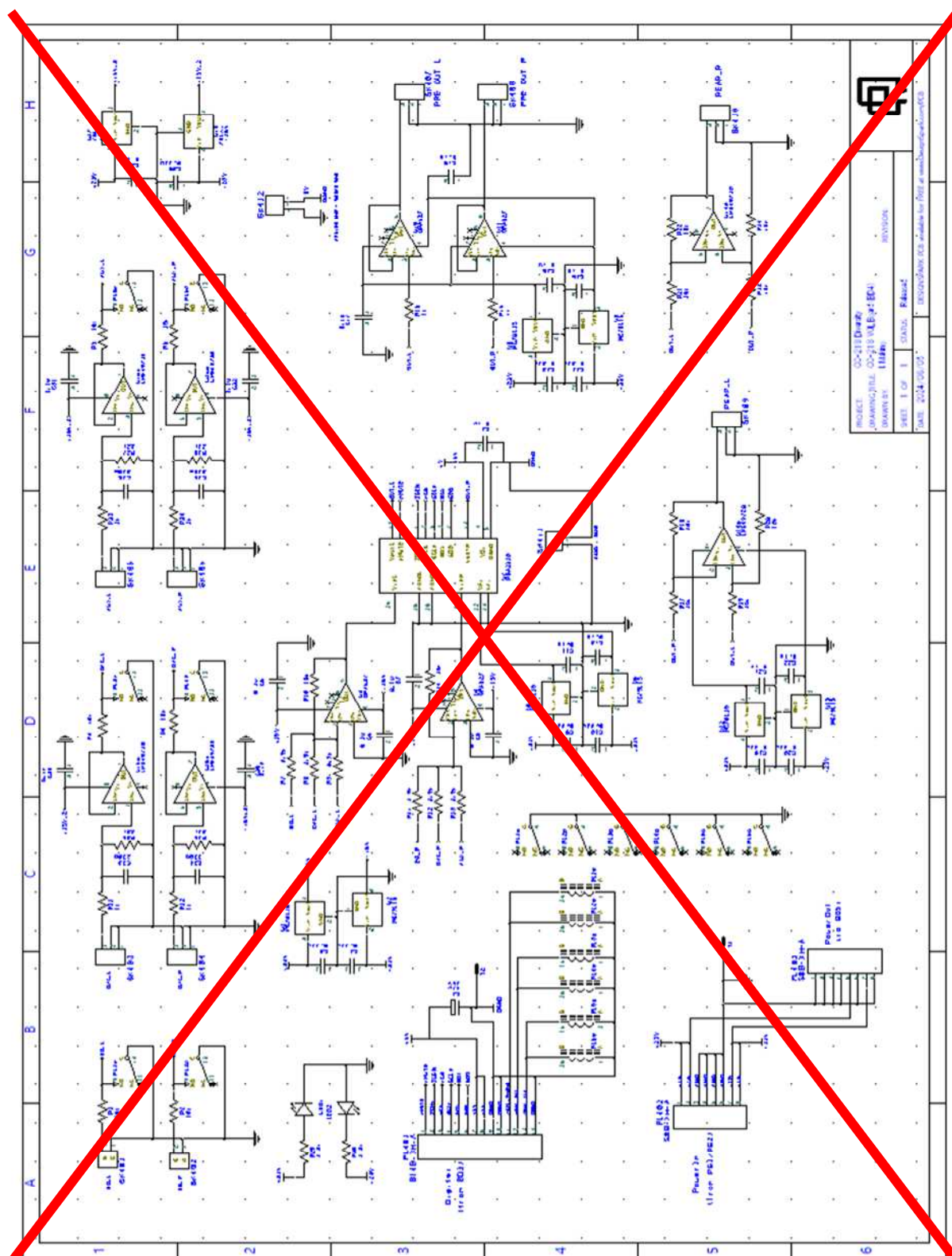
REAR\_L only

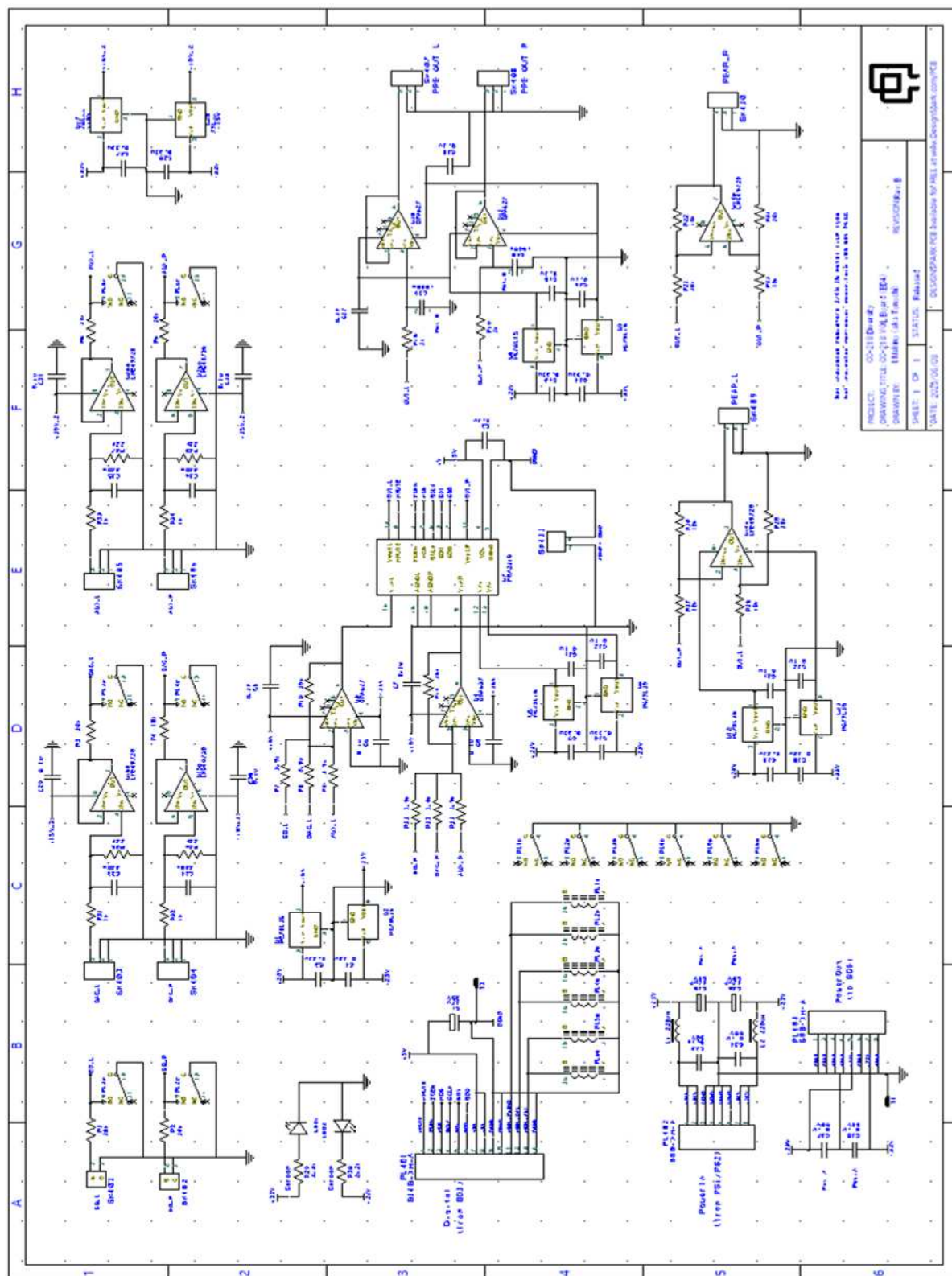


I quit simulation of Matrix here, because its SQ is not important.

For the latest schematic, see ~~CC 218\_VOL - Schematic.pdf~~ **CC-218\_VOL\_B - Schematic.pdf**.

2025/03/21





## Rev.A

LC 1st-order LPF added to DC power input:

L: 220uH (L1~2), C: 47uF (C35~36)

$f_c = 1.5\text{kHz}$

## Rev.B

CR 1st-order LPF added to output buffer:

C: 1000pF (C39~40), R: 1k ohm (R15~16)

$f_c = 160\text{kHz}$

Power Dissipation

2024/12/20

\* Current dissipation estimate

Device	Qty	Current dissipation		Total current dissipation	
		V+	V-	+23V	-23V
LME49720	3	12. 0mA	12. 0mA	36. 0mA	36. 0mA
OPA627	4	7. 0mA	7. 0mA	28. 0mA	28. 0mA
PGA2310	1	10. 0mA	10. 0mA	10. 0mA	10. 0mA
LED	1	10. 5mA	10. 5mA	10. 5mA	10. 5mA
Total				84. 5mA	84. 5mA

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